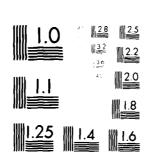
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FEEDBACK CONTROL FOR FUNCTIONAL ELECTRICAL STIMULATION OF PARALYZED MUSCLE

CORY D. CARROLL, 2nd Lt, USAF

MARCH 1981

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The experiments reported herein were conducted according to the "Guide for the Care and Use of Laboratory Animals, "Institute of Laboratory Animal Resources, National Research Council.

This report has been reviewed by the Office of Public Affairs (PA) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

HENNING E. VON GIERKE

Director

Biodynamics and Bioengineering Division

Air Force Aerospace Medical Research Laboratory

H. E. van Gichn

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Block 20. Abstract (cont'd)

posture control during locomotion is eliminated because of the support system of the harness. During locomotion in the harness, electromyographic activity of the essential hindlimb muscles were recorded with the corresponding position information from the harness. These data along with anatomical models of the leg allowed isolation of six "essential" muscles: iliopsoas, semimembranosus, vastus lateralis, biceps femoris, tibialis anterior, and gastrocnemius. Using only these six muscles, locomotion can theoretically be achieved while the cat is in the harness system. From the EMG data, initial activity of the essential muscles during locomotion was obtained and plotted against the cat step cycle.

FEEDBACK CONTROL FOR FUNCTIONAL ELECTRICAL STIMULATION OF PARALYSED MUSCLE

THESIS

Presented to the Faculty of the School of Engineering of the Air Force Institute of Technology

Air University

in Partial Fulfillment of the

Requirements for the Degree of

Master of Science

Ву

Cory D. Carroll 2/Lt. USAF

Graduate Electrical Engineering

December 1980

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PREFACE

I wish to show my appreciation to my advisor, Dr. Lynn E. Wolaver along with Dr. Matthew Kabrisky, both of the Air Force Institute of Technology, and to Dr. Jerrold S. Petrofsky, Wright State University, for their enthusiasm and advice throughout this project. A special thanks is given to Capt Arthur J. Nestle, formerly assigned to Biodynamic Effects Branch (BBD), Biodynamics and Bioengineering Division of the Air Force Aerospace Medical Research Laboratory (AFAMRL), and Lt Edward P. France for their support and insight in coordinating the efforts of the many agencies that were involved with this thesis. The AFAMRL Veterinary Sciences Division (AFAMRL/VS) provided the space for the experiments, and the personnel of both AFAMRL/VS and AFAMRL/BBD were extremely cooperative during the experimental work. Additional thanks are given to the AFIT shop, specifically, Mr. Russ Murry for actual construction of the harness. The excellent medical illustrations in this thesis were done by Heidi Gierard whose patience was tested by my constant interruptions

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FEEDBACK CONTROL FOR FUNCTIONAL ELECTRICAL STIMULATION OF PARALYZED MUSCLE

I. Introduction

Background

Disruption of normal neural pathways because of spinal injury results in paralysis below the level of the injury. Although the central command is no longer present to the alpha motor neuron pool below the level of the injury, if the cell bodies of these neurons have been undamaged the motor units remain healthy and unharmed (Guttman, 1976). However, the muscle fibers will decrease in size because of disuse atrophy. In about six months to two years the muscle will be atrophied to approximately one-fourth normal size and the muscle fibers will have been replaced mainly by fiberous tissue (Guyton, 1976). Thus, although healthy motor neurons and muscles are present, the individual remains paralyzed, often for life, due to the absence of central command. Considering that the average patient incurring spinal injury is between 31 and 36 years of age (Smart and Sandurs, 1976) and the increasing longevity of these patients, it has become very important to provide a means of mobility to allow them to move in their environments.

For the paraplegics, the wheelchair has been the most commonly used means of mobility. With the use of specially designed automobiles that can be operated by hand controls, the wheelchair patient is allowed an additional degree of freedom in their environments. Unfortunately, the life style of these patients is still very restrictive. In

addition, psychological problems arise because of the paralysis of their bodies.

Restoring mobility by replacing the lost central command to the alpha motor neurons with direct electrical stimulation of the muscle is a viable alternative to the wheelchair. It is important to realize that direct electrical stimulation can only be used when the cell bodies of the alpha motor neurons remain uneffected by the injury. If these cell bodies are destroyed, the motor neurons die and the muscle suffers irreversible denervation atrophy (Guttman, 1976; Debowitz and Brooke, 1974). By electrically stimulating both agonist and antagonist muscles, the stability required for postural control along with restoration of both hand and leg motion can be achieved (Crochetiere et al., 1967; McNeal et al., 1969; Milner et al., 1970; Kiwerski, 1973; Rehersek and Vodovnik, 1973; Petrofsky, 1978 a, b; Solomonow et al., 1978).

An inovative technique involving stimulation of the motor nerve itself rather than the muscle has been suggested by Petrofsky (1978 a,b,c) and Solomonow (1978). This technique offers the advantage of lower stimulation currents and voltages than those needed with intramuscular electrodes or electrodes placed directly on the skin. However, developing a stimulating system that will, (a) exert a fine control over the tension developed by paralized muscle during isometric contraction, (b) control the velocity of contraction enabling a coordinated movement of limbs, and (c) stimulate the muscles in a manner that will not rapidly fatigue the muscle, is an extremely complicated task that must be achieved before the lame can walk.

Purpose

This thesis is concerned with the design and construction of a mechanical harness that will attach to the rear limbs of a cat and act as a feedback device to a computer. The harness will measure the position and velocity of movement of the animal's joints and extremities. Precise positioning of the harness is essential since the computer must have accurate position information in order to compare the actual motion to the desired, predetermined motion of the limb. Restrictive aspects of the harness has been kept to a minimum thus allowing normal forward and backward movement of the leg. Because of the complexity of this project the lateral motion of the leg is limited by the harness.

In addition to construction of the harness, the minimum number of muscles needed for two dimensional movement (i.e., forward and backward) of the leg was determined. This reduction of required muscles simplifies the controlling program required for the stimulation process. Determination of the essential muscles was accomplished by forming anatomical models of the cat's mechanism for walking. The muscles in the leg contributing the essential function of basic locomotion were isolated and those used for lateral movement and rotational functions were ignored.

Electrodes were then implanted in the "essential" muscles and the signals produced by the central nervous system (CNS) during locomotion

[†]The term basic locomotion is defined as the two dimensional supported gait caused when the cat is confined in the harness assembly.

in the harness were recorded. Six muscles were eventually chosen that theoretically supply the needed control for basic locomotion. The sequence of activity of the electromyogram allowed the development of an initial stimulation pattern of each muscle during the gait cycle.

Scope

The work presented in this thesis is part of a project conducted by Jerrold S. Petrofsky, professor of Physiology and Bioengineering at Wright State University. Formally defined as functional electrical stimulation of paralyzed muscle, the end goal of this project is to have a cat walk under its own power after central nervous control to its rear limbs has been replaced by an external computer controlled stimulus. The domestic cat was chosen because of the large amount of biochemical, biomechanical and histological data compiled from previous work. In addition, the endurance and fatigue characteristics in the muscle of a cat closely resemble those of man. The concept of external control concerns the paraplegic community since success would allow use of the patient's own muscles for basic tasks.

II. Muscle Anatomy and Physiology

General Review

Muscles move the limbs and other parts of an animal's body. Each joint of the skeleton in enveloped by a loose capsule and between the two respective bones is the joint cavity. On the sides of each capsule are strong fibrous ligaments that keep the joints from pulling apart. The orientation of the ligaments around the joint defines the motion of the joint. Often the ligaments are only on two sides of the joint which allows the joint to move freely in one direction but restricts motion in another direction. Other joints, particularly those involving the spine, hips and shoulders, not having very restrictive ligaments, can move in almost any direction; that is, they can bend forward, backward, and to either side, or they can even be rotated. In these instances, loose ligaments merely limit the degree of motion to prevent excessive movement in any one direction. For the rear limb of the cat, the knee joint bends in only one direction, the ankle in two, the hip joint in two directions plus an additional rotary motion. Generally, at least two muscles are available for each motion that the ligaments of a joint allows; one for each of the two directions of movement. In the case of movement at the knee joint, for instance, one major muscle is on the front and several muscles are on the back of the joint. There is a similar arrangement of muscles anteriorly (to the front) and posteriorly (to the rear) about the ankle, except that the ligaments of the ankle allow the ankle joint to move from side to side and additional muscles are available to provide the sideway movement.

All skeletal muscles of the body are made up of numerous muscle fibers ranging between 10 to 80 microns in diameter. In most muscles the fibers extend the entire length of the muscle, and except for about two percent of the fibers, each of those is innervated by only one nerve ending located near the middle of the fiber (Guyton, 1976). The cell membrane of the muscle fiber is called the sarcolemma. At the ends of the muscle fibers the surface layers of the sarcolemma fuse with tendon fibers. The tendon fibers collect into bundles to form muscle tendons which attach to the bones.

Each muscle fiber contains several hundred to several thousand myofibrils, which are illustrated by the small dots in the cross sectional view of Figure 1. Each myofibril in turn has, lying side-by-side, about 1500 myosin fibrils and two times this many actin filaments (Guyton, 1976). These filaments, shown in Figure 2, are large polymerized protein molecules which are responsible for muscle contraction.

The mechanism of contraction is not completely understood but what is known is that the crossbridges of the myosin filament are attracted to the actin filament and some sort of wrenching action by the cross-bridges causes contraction (Wolaver, 1979). Under resting conditions, the reaction between the actin and myosin filaments is inhibited, but when an action potential travels over the muscle fiber membrane calcium ions are released into the sarcoplasm. (The myofibrils are suspended inside the muscle fiber in a matrix called sarcoplasm, which is composed of the usual intracellular constituents.) These calcium ions allow reaction of the filaments to take place and contraction begins. The

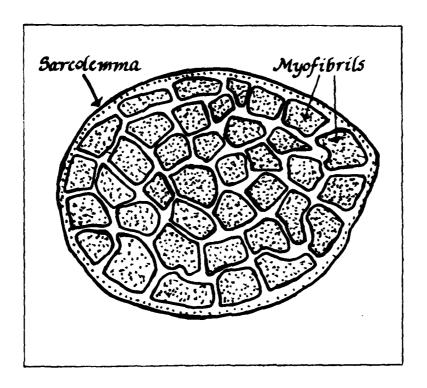


Figure 1. Cross Sectional View of a Skeletal Huscle Fiber

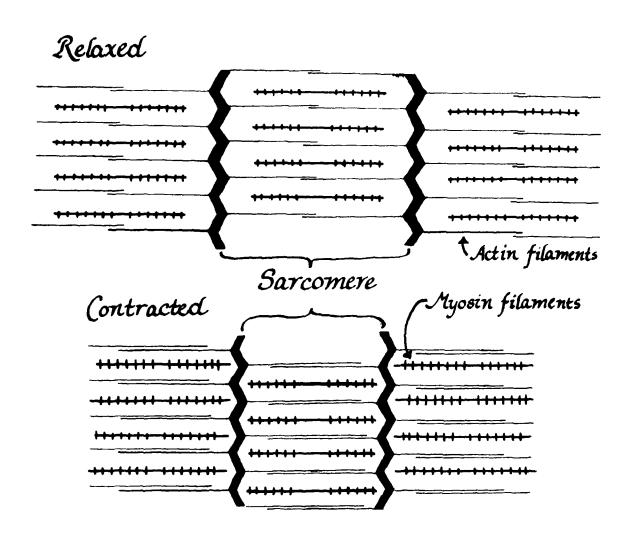


Figure 2. Relaxed and Contracted States of a Myofibril

energy needed for the contraction process is derived from the breakdown of adenosine triphosphate (ATP) to adenosine diphosphate (ADP) (Guyton, 1976).

Innervation

Muscle contraction is controlled by the central nervous system (CNS). Action potentials created by the CNS are transmitted to the specific muscles through the motor portion of the nervous system. Nerve bundles, which carry the signals developed by the CNS, are continually branching, with those branches innervating specified tissue. An illustration of muscle innervation is shown in Figure 3.

The nerve bundle has two means by which it can transmit signals of different strengths. These are (1) to transmit impulses simular taneously over varying numbers of nerve fibers, which is called spatial summation, and (2) to transmit impulses in a slow or fast rate over the same fiber, which is called temporal summation. As an example of spatial summation, if 100 nerve fibers are connected between the spinal cord and a foot muscle, stimulation of one of these fibers will cause only a weak response in the muscle, but simultaneous stimulation of all 100 fibers will cause a strong contraction. Obviously, any number of fibers between 1 and 100 can be stimulated at a time allowing for a fine gradation of contraction force (a process called recruitment).

Temporal summation means changing the strength of a signal by varying the rate of the impulses along the same fiber. If one impulse is transmitted each second, the muscle contracts weakly, but if the impulse rate is varied, the strength of contraction will be proportional

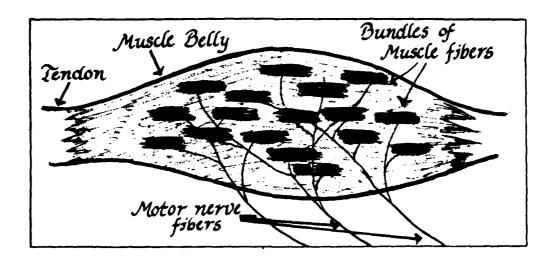


Figure 3. Nuscle Innervation

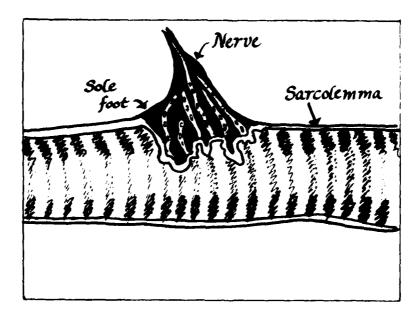


Figure 4. The Meuromuscular Junction

to the rate of stimulation (rate coding). (The upper bound on the impulse rate is determined by the refractory period of the fiber.)

Ordinarily the nerve trunk transmits signals of different strengths by a combination of both the spatial and temporal methods (Guyton, 1974).

Skeletal muscle fibers transmit impulses exactly as nerve fibers do. The normal velocity of transmission in skeletal muscle fibers is about 5 meters per second in contrast to 50 to 100 meters per second in the very large myelinated nerve fibers (Guyton, 1974). Because large myelinated nerve fibers control skeletal muscle, conduction velocity averages 60 meters per second. A signal, therfore, travels from the brain to the muscle extremely rapidly but then decreases in velocity more than 10-fold as it is conducted, across the muscle itself (Guyton, 1974).

The connection between the end of a large nerve fiber and a skeletal muscle fiber is called the neuromuscular junction. As stated proviously, each skeletal muscle fiber is usually supplied with at least one neuromuscular junction but rarely more than one. The neuromuscular junction is illustrated in Figure 4.

Lever Systems

Another factor which determines the force of movement is the manner in which the contracting muscle is attached to the skeletal system. The structure of the joint limits the directions that the corresponding bones can move. The mechanism for which motion of limbs is attained is that

of the cat's rear foot by contraction of the gastrocnemius muscle.

Referring to Figure 5, the fulcrum of the lever system is at the ankle and the insertion of the achilles tendon is on the end of the calcaneus bone. Contraction of the gastrocnemius pulls on the calcaneus which rotates the foot toward the ground around the ankle. To support a 5 lb. load at the knee, while in a normal standing stance, the gastrocnemius must produce a 19 lb. contraction force.

Every muscle of the body has its own peculiar shape and length that suit it to its particular function. The muscles of the buttocks are extremely broad but do not contract a long distance. They provide tremendous force for movement at the hip joint, and even a very slight distance of movement at this joint can cause tremendous movement at the foot. At the other extreme, some muscles of the anterior thigh are very long and can shorten a major distance along the thigh, pulling the shank upward at the knee joint and flexing the thigh at the same time.

Feedback

Kinesthesia is the conscious recognition of the orientation of the different parts of the body with respect to each other as well as the rates of movement of the different parts of the body. These functions are supplied mainly by extensive sensory endings in the joint capsules and ligaments.

Figure 6 illustrates the excitation of seven different nerve fibers leading from separate joint receptors in the capsule of a cat's knee joint. Note that at the 180 degrees of joint rotation one of the

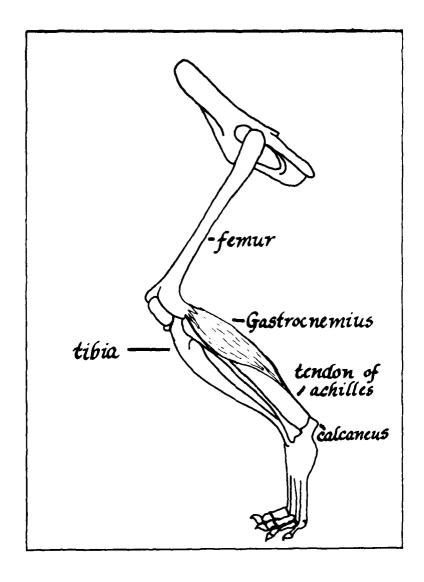


Figure 5. Lever Arm System of the Gastroccemius

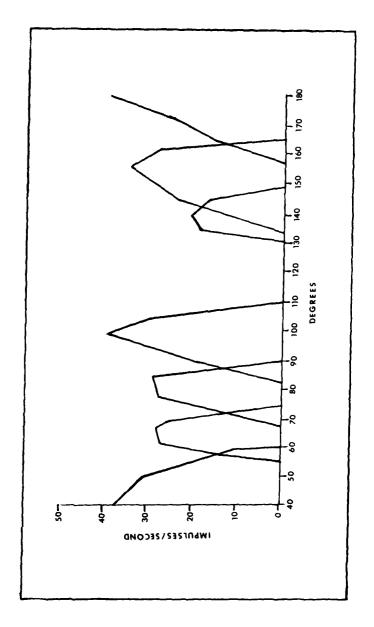


Figure 6. Kinesthetic Signals from the Knee of a Cat at Different Degrees of Rotation (Nodified from Sko_land: Acta Physiol. Scand., Suppl. 124,36:1, 1956)

receptors is stimulated; then at 150 degrees still another is stimulated; at 140 degrees two are stimulated, and so forth. The information from these joint receptors continually feed back the momentary rotation of the joint to the CNS. That is, the rotation determines which receptor is stimulated and how much it is stimulated, and from this the brain knows how far the joint is bent.

Rate of rotation is presumed to be used in this feedback control. Small amounts of specialized nerve endings called pacinian corpuscles are found in the tissue around the joints and have the property of rapid adaptation to the movement of the joints. The mechanism is as follows; the specialized nerve endings produce a strong stimulus when the joint is moved and then fades to a lower steady-state signal within a fraction of a second. This same type of signal is also produced by the position receptors but the difference between initial stimulus and the steady state signal is not as drastic. Nevertheless, this early overshoot in receptor stimulation is directly proportional to the rate of joint movement and is believed to be the signal used by the brain to discern the rate of movement (Guyton, 1976).

Kinesthetic signals are transmitted by the sensory nerve fibers which carry signals very rapidly to the spinal cord and to the brain. This rapid transmission of kinesthetic signals is particularly important when parts of the body are moving rapidly, because it is essential for the nervous system to "know" at each small fraction of a second the exact locations of the different parts of the body; otherwise one would not be capable of controlling further movements.

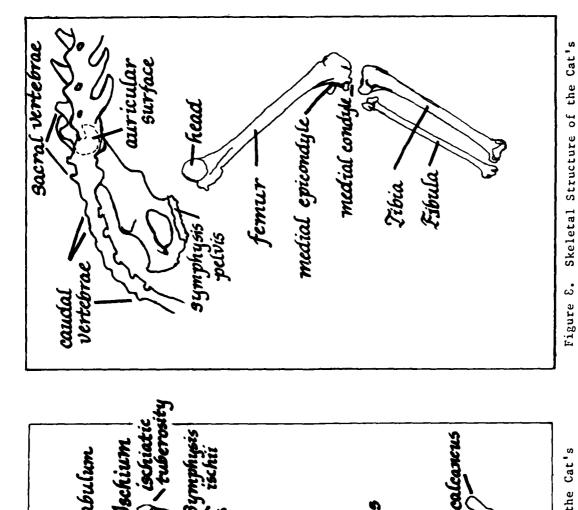
III. Muscles of the Cat's Rear Limbs

This section provides a purely anatomical description of the muscular structure in the cat's rear limb. The following sections will contain the description, origin, insertion and action of each muscle with corresponding figure.† Muscles of the foot along with assorted small muscles of the limb, whose function does not contribute to the gross movement of the limb, are not included.

Skeletal Structure

The skeletal structure of the cat's left leg is shown in Figure 7 and 8. Figure 7 illustrates the lateral aspect (side view) while Figure 8 shows the medial aspect (opposite to side view). These figures will be helpful for visualizing origin and insertion points of the various muscles presented in the following figures.

[†]Construction of the anatomical illustrations used material presented by Greenblatt (1954), Crouch (1969) and Donnersberger et al., (1975).



Symphysis

femur

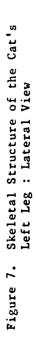
Ischium

greater trochantes

acetabulum

Wing

Hium



Tibia'

Fibula

Left Leg: Medial View

lateral epicondyle

Q d

trochante

interosseous space

Superficial Muscles of the Thigh

Medial Aspect (See Figure 9)

 Sartorius - large band of muscle extending from the crest and ventral border of the ilium to the patella.

Origin - crest and ventral border of ilium.

Insertion - proximal end of tibia and patella.

Action - adducts and rotates the femur and extends the shank.

2. Gracilis - a wide, flat muscle covering most of the thigh below the sartorius.

Origin - ischial bone and pubic symphysis.

Insertion - tibia and fascia of shank.

Action - adducts the leg.

 Iliopsoas - a triangular shaped muscle which is caudal to the sartorius.

Origin - anterior iliac crest.

Insertion - lesser trochanter of femur.

Action - adducts the femur.

Lateral Aspect (See Figure 10)

4. Gluteus medius - a relatively large muscle in the cat and somewhat triangular.

Origin - crest and lateral surface of ilium.

Insertion - greater trochanter of femur.

Action - aids in abducting the thigh.

5. Gluteus maximus - triangular mass immediately posterior to the medius.

Origin - last sacral and first caudal vertebrae.

Insertion - fascia lata and greater throchanter of femur.

Action - abducts thigh.

6. Caudofemoralis - band of muscle posterior to gluteus maximus and anterior and dorsal to biceps femoris.

Origin - second and third caudal vertebrae.

Insertion - patella.

Action - abducts thigh and extends shank.

7. Biceps femoris - very broad muscle posterior to the fascia lata.

Origin - tuberosity of ishium.

Insertion - patella, tibia, and shank fascia.

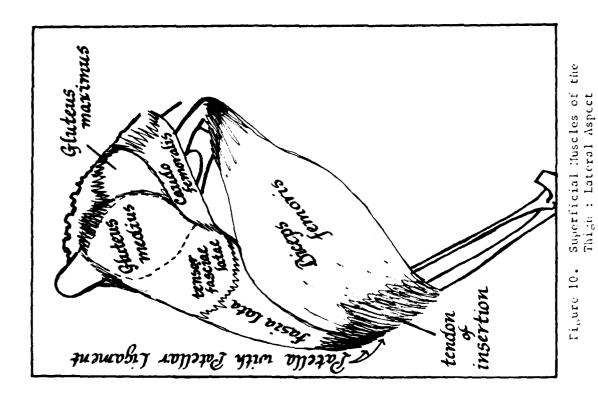
Action - abducts thigh and flexes shank.

8. Tensor fasciae latae - triangular mass of muscle anterior to the biceps femoris.

Origin - ilium and fascia.

Insertion - fascia lata.

Action - tightens fascia la ...



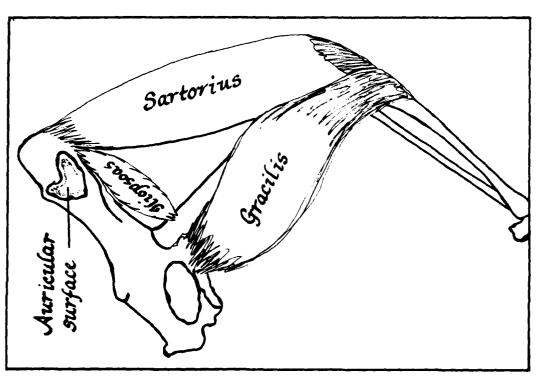


Figure 9. Superficial Muscles of the Thigh: Medial Aspect

Deep Muscles of the Thigh

Lateral Aspect (See Figure 11)

1. Vastus Lateralis - this large muscle lies under the fascia lata and covers the anterolateral surface of the thigh.

Origin - greater trochanter and shaft of femur.

Insertion - patella.

Action - extends shank.

2. Semitendinosus - a large band of muscle covering the posteromedial border of the popliteal fossa.

Origin - ischial tubrosity.

Insertion - medial side of tibia.

Action - flexes the shank.

Medial Aspect (See Figure 12)

3. Rectus femoris - narrow band of muscle on the front of thigh medial to the vastus lateralis.
It lies beneath the sartorius.

Origin - ilium, anterior to acetabulum.

Insertion - patella and patellar ligament.

Action - extends shank.

4. Vastus medialis - large muscle on medial surface of thigh, posterior to the rectus femoris. It is covered by the sartorius.

Origin - shaft of femur.

Insertion

- patella.

Action

- extends shank.

5. Adductor femoris - large triangular mass of muscle

Origin

- ischial and pubic symphysis.

Insertion

- shaft of the femur.

Action

- adducts and extends thigh.

6. Semimembranosus - a large muscle posterior to the

adductor femoris.

Origin

- posterior edge of ischium.

Insertion

- medial epicondyle of femur.

Action

- extends thigh.



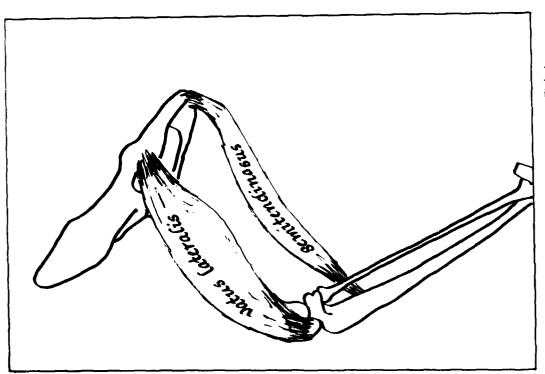


Figure 11. Deep Muscles of the Thigh: Lateral Aspect

Muscles of the Shank

Lateral Surface (See Figure 13)

Gastrocnemius - a large muscle mass on the dorsal surface of the foreleg.

Origin - lateral and medial condules of femur.

Insertion - tendon of Achilles on calcaneus bone.

Action - extends foot.

2. Soleus - small band of muscle lying next to the lateral head of the gastrochemius.

Origin - lateral surface of the head of the fibula.

Insertion - calcaneus by tendon of Achilles.

Action - extends foot.

3. Peroneus - elongated band of muscle occupying the fibular aspect of the shank.

Origin - lateral aspect of the head of the fibula.

Insertion - bases of the metatarsals and phalanges.

Action - extends foot and assists with plantar flexion. Prime mover for eversion of foot.

4. Tibialis anterior - a slender miscle situated on the anterolateral aspect of the tibia.

Origin - proximal lateral surface of the tibia and corresponding portion of the interosseous membrane which joins the tibia and fibula.

Insertion

- base of first metatarsal.

Action

- dorsiflexion and inversion of foot.

 Extensor digitorum - slender, tapered muscle, which must longus

be separated from the tibialis

anterior, which overlaps it.

Origin

- lateral epicondyle of femur.

Insertion

- phalanges.

Action

- extends phalanges.

Medial Surface (See Figure 14)

6. Flexor digitorum longus

- the first head (6a) is covered partly by the soleus and lies against the central surface of the tibia and fibula. The second head (6b) lies between the long head and

Origin

- first head - tibia.
second head - fibula and fascia.

Insertion

- in common by a tendon to the digits.

medial aspect of the gastrocnemius.

Action

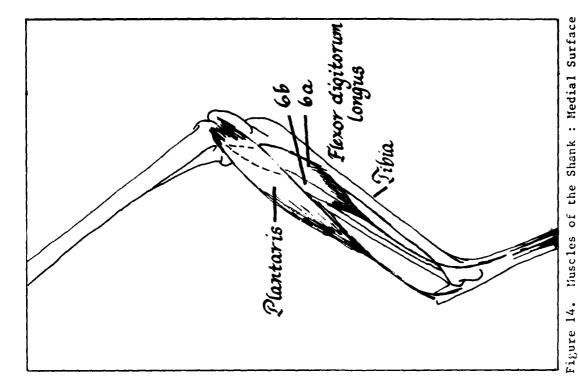
- flexes foot.

7. Plantaris

- the two heads of the gastrocnemius muscle meet behind an indistinct line. If the two heads are separated, a strong round muscle will be revealed enclosed by the two heads. This muscle is the plantaris. Origin - patella.

Insertion - calcaneus and phalanges.

Action - flexes phalanges.



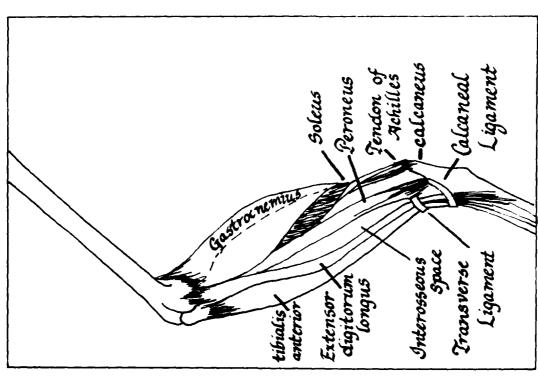


Figure 13. Huscles of the Shenk: Lateral Surface

IV. Definition of the Cat Step Cycle

A common method of examining the cat step cycle divides the cycle into two phases, the swing and stance phase. Each of these phases is further divided into two more phases which is illustrated in Figure 15. The flexion (F) phase begins as the foot is thrust off the ground at which time there is a beginning flexion at hip, knee and ankle joints. This phase ends as the extension begins in the knee and ankle. These movements of limb flexion and early extension (\mathbf{E}^1) comprises the swing (foot off the ground) phase of the step cycle. The stance (foot on the ground) phase involves progressive extension of the hip at increasing speed. During the second phase (E2) the knee, ankle and metatarsophalangeal (hindpaw structure) joints yield under the animal. This yield is slight in walking but become quite pronounced as the animal converts to high speed locomotion. The notation of the arrows to separate the swing from the stance phase and the dots used to separate F from E^1 and E^2 from E^3 (See Figure 15) will be used in subsequent figures.

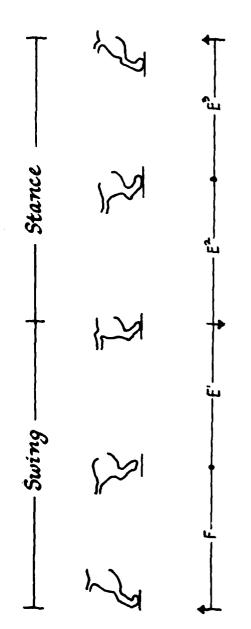


Figure 15. Phases of the Cat Step Cycle

V. Reduction of Muslce Groups

Controlling the motion of the cat's leg is extremely complicated. This can be visualized by the intricate network of the controlling muscles illustrated in Chapter III. Stimulation of the muscles normally used during locomotion by an external computer would require an enormous software routine. In addition, the task of surgically implanting the corresponding muscle stimulators developed by Petrofsky is not feasible at this time. These two problems will eventually be solved, but for initial attempts to control locomotion, a functional gait cycle can be achieved by concentrating on "essential" muscles.

The criteria for finding the essential muscles is well defined because of the use of the harness system.† Although the cat has a normal gait in the harness, the lateral motion, along with rotational characteristics of the leg, has been virtually eliminated. These two restrictions of the leg motion allow for reduction of the number of needed muscles for locomotion. A further aspect of the harness implementation that permits this reduction is that of body support. With the sling and tail clamp in use, the cat's haunches are supported, and therefore, the problem of posture control during locomotion is greatly simplified.

With the above criteria, a purely anatomical representation of the muscle structure in the leg was analyzed. From this analysis, a "first

The harness system is described in Chapter VI.

TABLE I

Nonessential Muscles

luscle

Reason Eliminated

Thigh:

Sartorius produces rotational motion

Gracilis produces lateral motion

Gluteus medius produces lateral motion

Gluteus maximus produces lateral motion

Caudofemoralis produces lateral motion

Tesor Faschae Latea small contribution to gross movement

Vastus Medialis secondary to vastus lateralis

Adductor femoris produces lateral motion

Shank:

Soleus secondary to gastrocnemius

Peronus produces lateral motion

Extensor digitorum longus small contribution to gross movement

Flexor digitorum longus secondary to tibialis anterior

_cut" in the isolation of nonessential muscles was achieved. Table I lists the muscles eliminated and the reason.

A very good representation showing the location of the remaining muscles is shown in Figure 16 (Goslow, et al., 1973). The straight line length of the muscles depict the distance from the most proximal point of muscle origin to the most distal point of insertion. The presented muscle lengths include the length of tendon of origin and/or insertion. Table II explains the abbreviations used in Figure 16.

From the model shown in Figure 16, six muscles were isolated that theoretically produce the needed forces for locomotion in the harness. In all cases, the characteristic of pure flexion and extension were prime criteria in selection. Accessability of the muscles was included in the selection criteria. This included the ability to isolate the inner-vation and surgically implant the stimulating lead. The essential muscles finally selected are listed below:

Thigh flexor -- iliopsoas

Thigh extensor -- semimembranosus

Shank flexor -- biceps femoris

Shank extensor - vastus lateralis

Foot flexor -- tibialis anterior

Foot extensor -- gastrocnemius

Figure 17 shows the reduced model (refer to Chapter III for anatomical information of the muscles).

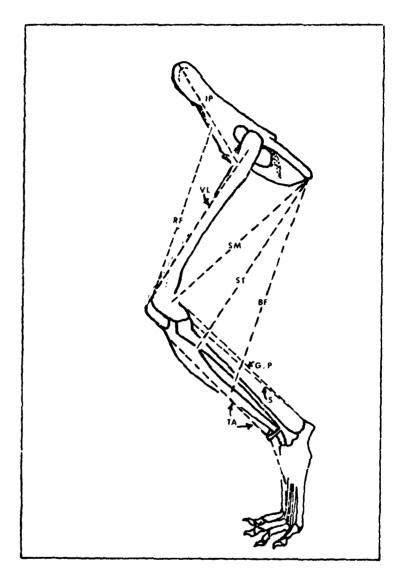


Figure 16. Model of the Major Muscles in the Leg

TABLE II

Anatomical Model Notation

Abbreviation	Muscle	Refer to Chapter III Figure #
SM	Semimembranosus	12
RF	Rectus femoris	12
BF	Biceps femoris	10
ST	Semitendinosus	11
G	Gastrocnemius	13
PL	Plantaris	14
VL	Vastus lateralis	11
16	Iliopsoas	9
S	Soleus	13
TA	Tibialis anterior	13

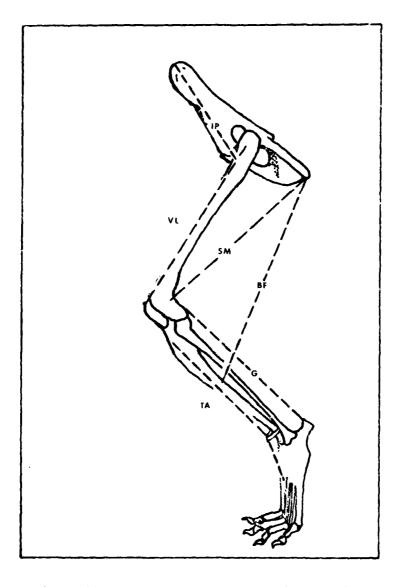


Figure 17. Reduced Hodel : Essential Muscles in the Leg

Verification of the action of the six muscles chosen was done by analysis of EMG data recorded with position signals from the harness.†

This data shown in Figure 18 exhibit the expected activity of the essential muscles. In both charts, the first three channels of the graph depict the harness signal. (The noise shown on the left hip signal in Figure 18a is due to a discontinuity in that potentiometer.)

The EMG waveforms shown in Figure 18 are the signals developed directly from the muscles. The absence of the usually characteristic spikes in EMG signals is because of the choice of recording parameters used in the collection of this data. These recording parameters and their influence on the EMG signals is discussed in Appendix 8.

Referring to Figure 18a, the gastrocnemius shows initial activity in the E^1 phase which corresponds to the preparation of foot placement. The tibialis anterior begins its activity during the E^3 phase and peaks at the lifting of the foot. This stimulation causes flexion of the foot during the swing phase.

Extension of the shank caused by the vastus laterals is accomplished during the swing phase, shown by the activity occurring during the F and E¹ phase. Flexion of the shank by the biceps femoris, shown in Figure 18b, occurs at the end of the E³ phase and continues throughout the swing phase.

Semimembranosus activity is developed in the E^1 phase and continue up to the end of the E^3 phase. The contraction of the semimembranosus

 $^{{\}ensuremath{^{\dagger}}}{\ensuremat$

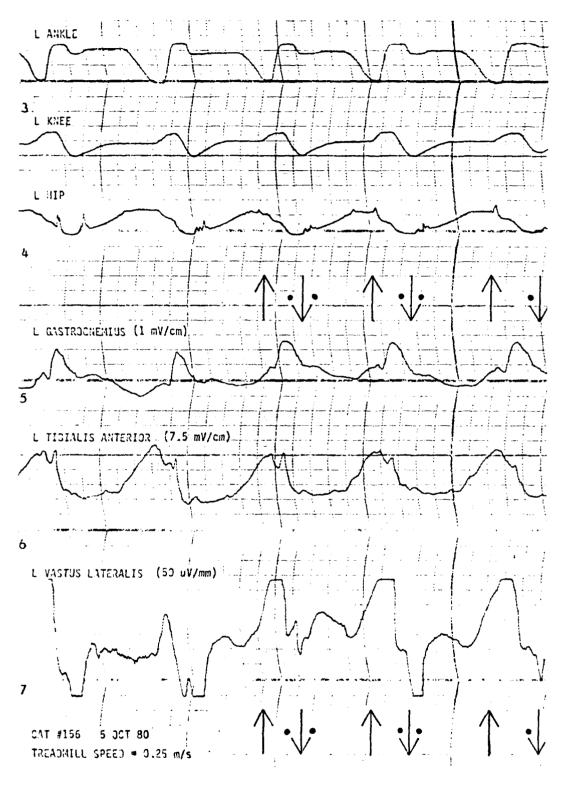


Figure 18. MIC Signals of Essential Muscles and Position Information

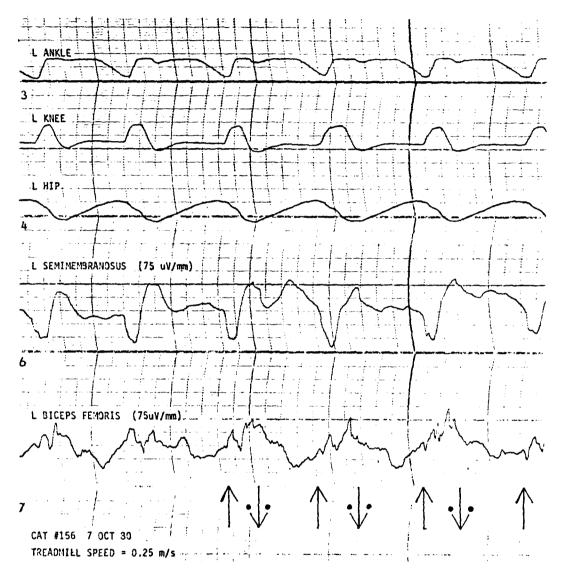


Figure 18b

extends the thigh while the foot is on the ground. Iliopsoas EMG signals are not included because of problems of electrode placement. However, Engberg and Lundberg (1968) recorded the EMG from the iliopsoas during a comparable walking speed. The iliopsoas signal displayed activity throughout the F and E¹ phase and develops thigh flexion during the swing phase.

Additional data were recorded for different treadmill speeds and is included in Appendix B.

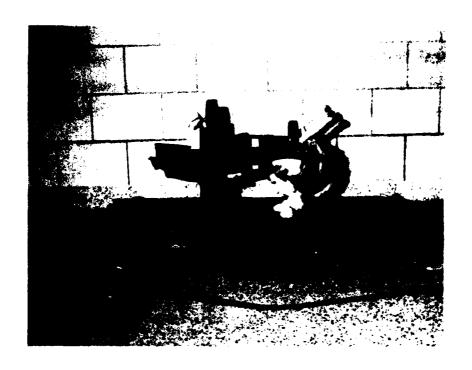
VI. Harness

Position feedback information of the cat's rear limbs during locomotion is developed by an external harness. The design criteria for the harness is listed below:

- 1) Support the animal's front torso.
- 2) Provide lightweight leg members that will noninvasively attach to the rear limbs.
- Restrict lateral movement of the rear leg and yet allow unrestrained forward and backward motion.
- 4) Allow for variation of physical size for different experimental animals.
- 5) Incorporate measuring transducers to provide position information while keeping the leg member system as lightweight and nonrestrictive as possible.

The physical system that fulfills the above constraints is shown in Figure 19. The harness assembly is bolted to the treadmill frame and allows free travel of the treadmill belt.

The treadmill belt is driven by a 1/8 hp variable speed motor. The speed of the belt is measured by a simple magnet switching device which counts the rotation of the driving cylinder. The motor produced a constant treadmill belt speed once set which ranged from zero to one meter per second. The roller system which the belt traveled over was modified by placing a section of plexyglas over the rollers. This modification eliminated the unevenness produced by the rollers and provided a hard flat surface for the cat to walk on.



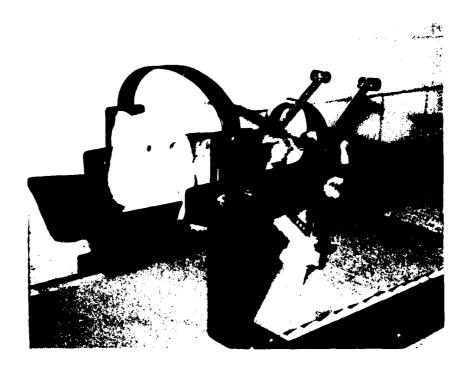


Figure 19. Harness Assembly

Mechanical Design

The support mechanism is incorporated to keep the pelvic area in a set location while the cat walks on the treadmill. This mechanism used a sling apparatus in which the cat's front paws and torso rests. Slits were initially cut into the sling to allow use of the front paws during locomotion. This modification produced an unfavorable result in that the cat would either drag all four limbs or use the front paws to stop the treadmill belt. With the front paws elevated, there is no significant difference in the gait of the rear limbs.

Aluminum rods provide the side support for the nylon material of the sling. These solid 1/4 in. diameter rods can be bent to conform the sling to the animal's shape. The sling mounting brackets allowed both vertical and horizontal adjustment along with the ability to tilt the sling apparatus. Tie-down straps are available to confine the cat on the sling. These straps were used only during the recovery period of the animal from the ketamine injection. Once walking, the cat seemed quite content to remain in the sling.

Positioning of the leg members is accomplished by the harness positioning arms. Shown in Figure 20, the positioning arms attached to the support frame and determined the vertical height of the cat's hindquarters above the treadmill. Dimensions of the support assembly are shown in Figures 20 and 21.

Actual measurement of the leg position is done by the leg members.

Information concerning the design of the leg members was obtained through videotape recordings of unencumbered cats walking on the treadmill.

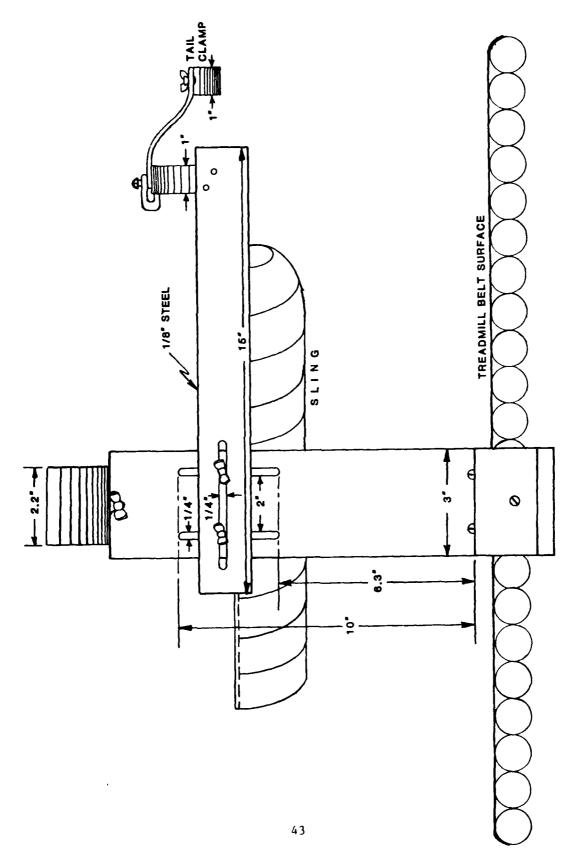


Figure 20. Harness Support System: Side View

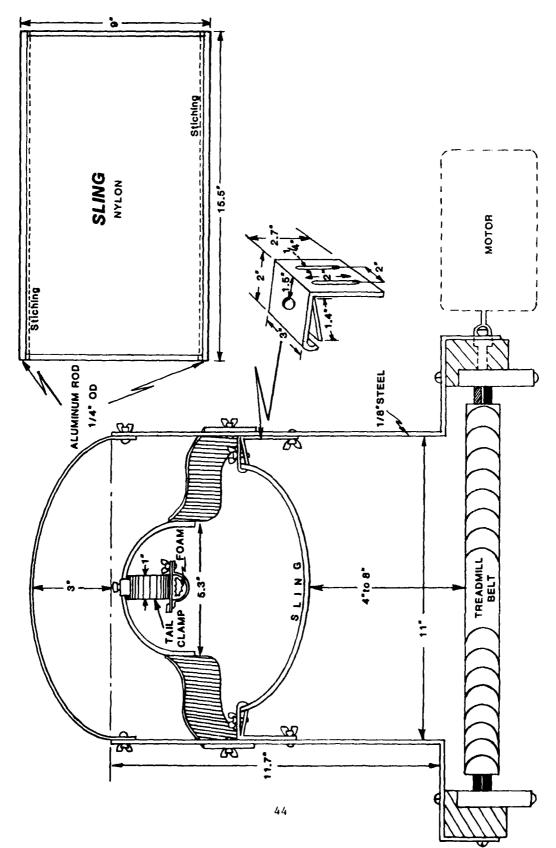


Figure 21. Harness Support System : Front View

A transparent enclosure shown in Figure 22 was placed over the treadmill to keep the animal on the treadmill belt. A grid system painted on one side of the enclosure provided a coordinate system for motion analysis. The result was used to specify the range of motion of the leg members. The film also provided a means for visual comparison of the gait cycle during unrestrained locomotion and during locomotion in the harness. Figure 23 illustrates the final design of the leg members.

The leg members correspond to the skeletal bones of a cat's leg.

They are defined as 1) the femur member, 2) the tibia member, and

3) the metatarsal member. Rotation of the leg members is at the same points of rotation of the limb, i.e., the hip, knee and ankle. Teflon washers used at the knee and ankle pivots reduced the friction and allowed free movement of the leg members.

The location of the hip pivot of the femur member is at the junction of the cat's femur into the ischium. Since the harness does not allow spinal arching, the cat's haunches need to be supported so that the hip pivot of the harness and the cat's hip joint will maintain the geometry desired in its preparation. To accomplish this support, a tail clamp was designed (See Figures 20 and 31). The tail clamp along with the sling assembly provides the needed support for hip positioning.

Attachement of the leg members to the cat's leg is done at the metatarsal member. A styrofoam pad which is contoured to the cat's foot provides the contact point. Velcro fasteners are used to strap the styrofoam piece to the foot. When attached, the leg members faithfully track the motion of the leg. In addition, the design criterion of

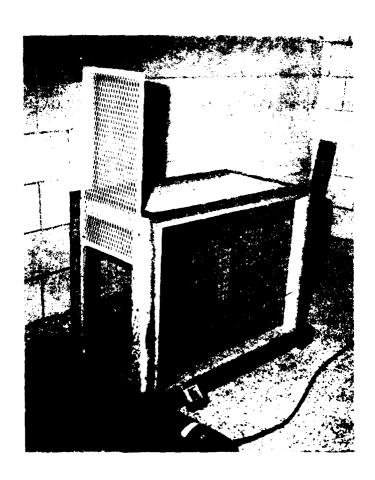


Figure 22. Transparent Enclosure with Grid Network

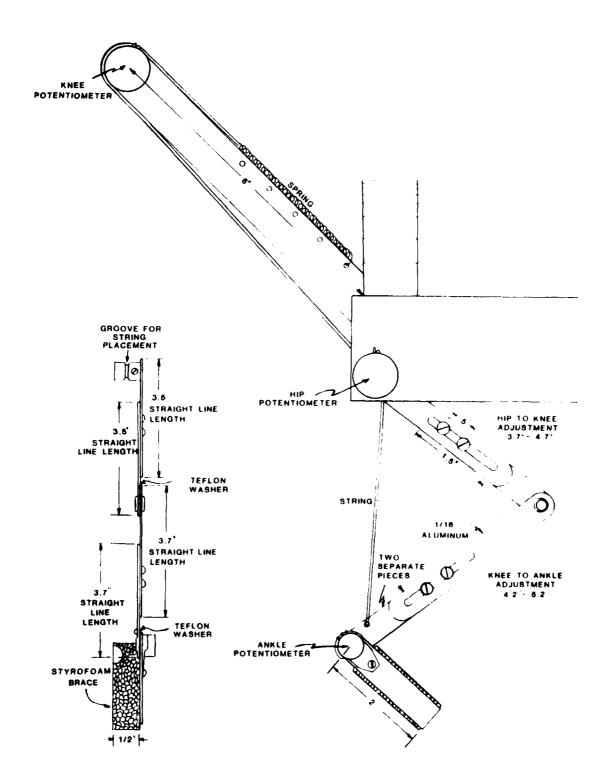


Figure 23. Harness Leg Members and Measuring Transducers

limiting the lateral or side-to-side movement of each leg is achieved with this system.

Position information for each joint is provided by potentiometers. Three potentiometers (pots) are used for each leg harness providing rotation information from the hip, knee and ankle joints. The size and weight of the potentiometers was a major design problem. To minimize the weight transferred to the cat, only the ankle pot is attached directly to the leg harness. A small $50 \, \mathrm{k}\Omega$ potentiometer attached at the ankle pivot measures the angle between the tibia member and the metatarsal member. Weighing only six grams, this device is well suited for placement on the leg harness. With this device included, the total weight of the leg harness is 40 grams. Both the hip and knee pots are attached to the support frame, and thus, no additional weight is applied to the leg harness.

With the weight constraint removed, 10-turn $20k\Omega$ potentiometers were used for the hip and knee measurement devices (10-turn pots were used because of ease of rotation and availability). The shaft of the hip pot supported the leg harness system. With the body of the pot attached to the positioning arms and the shaft attached to the femur member, movement of the thigh is measured.

Angular change in the knee joint is translated to the knee potentiometer using a string and pully system. As can be seen in Figure 23, a spring supplies the required tension to keep the string taut. The travel of the string around the rubber pully on the shaft of the knee pot measures the change in the knee angle. The law of

cosines defines this representation such that the knee angle can be expressed as:

Knee $\ell = \arccos[(F_{\ell}^2 + T_{\ell}^2 - S_{\ell}^2)/2F_{\ell}T_{\ell})]$

where; F_{ℓ} = length from knee pivot to hip pivot

 T_{ℓ} = length from knee pivot to insertion of string in the tibia member

 S_{ℓ} = length of the string measured from the hip pivot to its insertion in the tibia member.

This system for knee angle measurement provided an additional incidental improvement to this experiment. Because of the pulling force of the spring, the leg members impose a zero effective weight on the cat when in a standing stance. This system is, therefore, less restrictive than it would be if the full weight of the harness was transferred to the leg.

Electronics

The principle by which the potentiometers supply the position information is that of measuring the rotation of a specified member. A voltage divider circuit is created when a constant voltage is supplied across the potentiometer and the output voltage is taken from the pot wiper lead. Rotation of the pot's shaft causes a change in the resistance ratio and will change the output voltage. In this manner, a voltage level is produced that is proportional to the rotation of the pot shaft. The signals produced by the potentiometers are sent to the circuit shown in Figure 24. Each potentiometer signal travels through

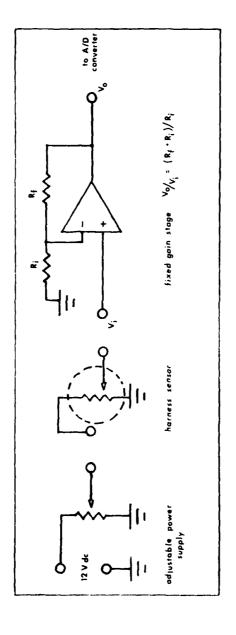


Figure 24. Schematic of Harness Circuit

its own circuit which provides two functions; 1) to allow for gain adjustment and 2) create a low impedance output signal.

Analog to Digital (A/D) converters will digitize the position signal produced by the potentiometers. To obtain maximum resolution from the converters, the voltage range corresponding to the leg motion must be identical to the input voltage range of the A/D. Trim potentiometers accomplish this adjustment by controlling the input voltage to the position pots. Since the circuit shown in Figure 24 produces a fixed gain for each signal, the input voltage is proportional to the output voltage. By physically positioning the leg members to their corresponding maximum travel, the output voltage can be adjusted to the desired level. Each potentiometer has independent adjustment capabilities. The individual parameters used in the complete harness circuit are listed in Table III.

The low impedance characteristic of the amplified output signal improves the accuracy of the A/D converters. Physically positioning the harness members and measuring the angle of the members and the corresponding output voltage from the potentiometers allowed the formulation of voltage-angle relationship. Figures 25, 26 and 27 show the voltage-angle relationship for the left leg harness. The data points in the figure represent the actual measured values. A best-fit curve was then traced to the data points. In each case, the curve produced a relationship that can be considered linear for all practical purposes. The small deviations from the linear relationship are caused by imprecise characteristics of the current position potentiometers.

TABLE III

Harness Circuit Compounds†

Channel	Angle Measured	Harness potentiometer	Gain
ı	right ankle	l-turn 50 kΩ	1.25
2	right knee	10-turn 20 kΩ	1.25
3	right hip	10-turn 20 kΩ	1.8
4	left ankle	l-turn 50 kΩ	1.25
5	left knee	10-turn 20 kΩ	1.25
6	left hip	10-turn 20 kΩ	1.8

the trim-pots used in the adjustable power supply were 10 k $\!\Omega_{\rm s}$. LM1458 operational amplifiers were used in the gain stage.

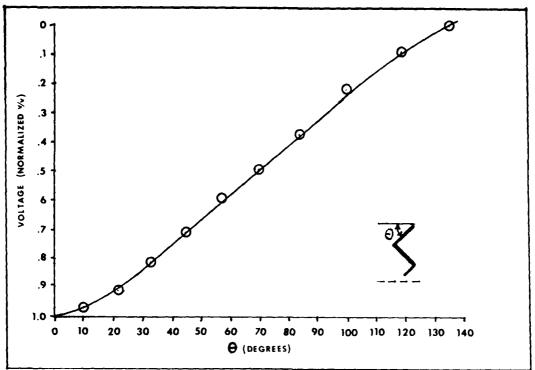


Figure 25. Voltage-Angle Relationship for the Left Hip

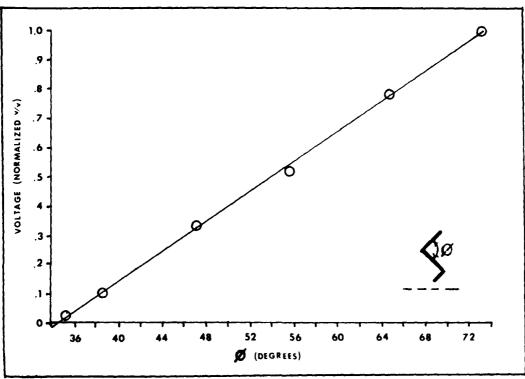


Figure 26. Voltage-Angle Relationship for the Left Knee

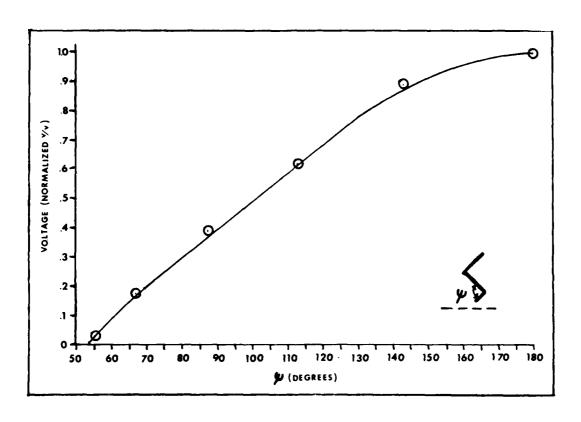


Figure 27. Voltage-Angle Relationship for the Left Ankle

Before actual interface with the A/D converters, high quality position pots will be substituted for the present units.

Sample output from the harness potentiometers is shown in Figure 28. For any instance in time, the position of each leg member can be calculated. As an example, the position of the leg members corresponding to the points A and B in Figure 28 are illustrated in Figure 29.

Calculating the angle relationship of leg members from the input voltage will eventually be accomplished through look-up tables in a computer. Binary numbers created by the A/D converters will correspond to specific angles of a joint. A simple precalibration routine will assign angle values to the binary numbers as follows. Minimum and maximum angles of each joint will be physically set and the corresponding output signals will be "locked on" by the computer. Using the linear relationship between the voltage output and angle, the routine will assign corresponding binary numbers to the intermediate angle values.

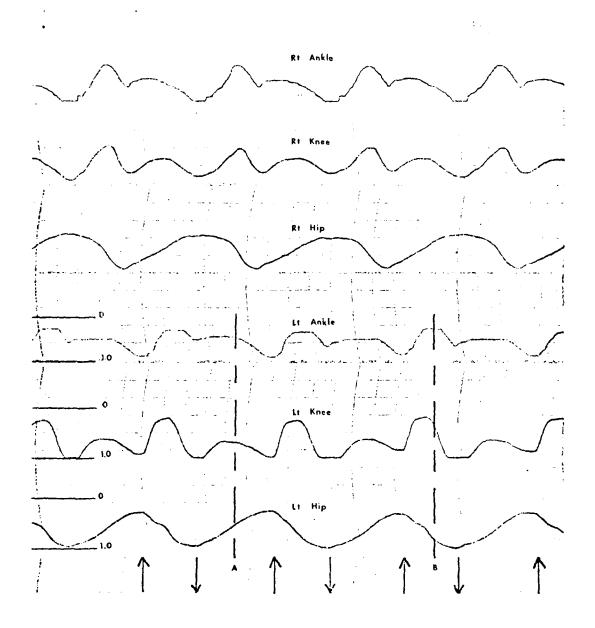
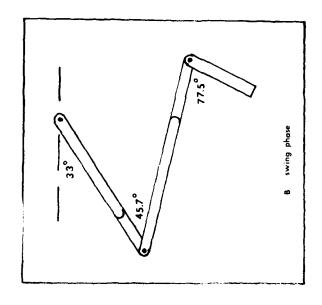


Figure 28. Sample Output From the Leg Marness



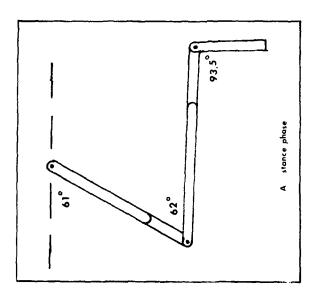


Figure 29. Example of Leg Newbers Position

VII. Experimental Procedures

Two adult cats weighing approximately 3.5 kg were selected for use in this project. Cat #156 was a male and cat #153 was a female. The cooperative nature of the animals was an essential part of this project. Not only did the cats have to voluntarily walk on a treadmill but do so while strapped in the harness assembly. Of the two cats chosen, only the male would copperate with the hardware. The electromyogram (EMG) data presented in this thesis was obtained from the male cat.

Preparation of the cat

Isolation of individual muscle activity during the step cycle was achieved by inserting silver electrodes into the muscle body. Two electrodes were implanted in the muscle to generate the EMG signal. The ground reference was supplied by a surface electrode applied to the upper hip area. Each experiment recorded the activity of three muscles in one leg along with the position information produced by the harness. Figure 30 shows a close-up photograph of placement of electrodes in the left leg in which the biceps femoris, gastrocnemius and tibialis anterior are the muscles under consideration. With the harness attached as shown in Figure 31, the electrode leads are undisturbed and interface with the electrode board of the recorder.

Alternating the leg used for the EMG data was done so that destruction of the leg tissue was kept to a minimum.



Figure 30. Placement of Electrodes for EMG Analysis



Figure 31. Harness and EMG Configuration

The electrodes inserted into the muscle are composed of a teflon coated silver wire (99.99% Ag). The silver wire has a 0.003 in outer diameter with a 0.0015 in coated layer of teflon providing the insulation. The wire is threaded through a 22ga 1 1/2in hypodermic needle. Using micro-tweezers, approximately 2mm of the teflon coating is stripped from the silver wire protruding from the needle tip. The bared silver is then bent into a hook which will lodge in the muscle when the needle is withdrawn. The opposite end of the wire is cut 5cm from the base of the needle and 2-3cm of teflon is stripped away in the same manner as before. The electrode and hypodermic needle is then sterilized using a gas sterilizer. Figure 32 shows the electrode and needle system prior to insertion.

Preparation of the cat involved complete shaving of both rear limbs, the lower back and pelvic area, forward to the middle of the rib cage. A 0.5cc intramuscular (IM) injection of ketamine is given prior to insertion of the electrodes. With the cat "knocked down", the leg to be used is scrubbed with a veterinary betadine solution.

Shortly after the ketamine is introduced, the hypodermic needle is inserted into the muscle under consideration. Two electrodes are inserted into the midsection of the muscle with the separation of the electrodes being approximately 3cm. The localization of the electrode was controlled before and after each session by electrical stimulation and palpation of the twitching muscle and its tendon. Additional verification of localization was accomplished during the experiment by comparison of the individual EMG signals to corresponding data presented by Engberg and Lundberg (1968).



Figure 32. Electrode and Hypodermic Needle Prior to Insertion

Special care is needed when securing the exposed electrode to the skin. Because of the slippage of the skin over the muscles, electrodes are easily dislodged if slack in the exposed wire is not provided. The exposed silver is then soldered (low-temperature) to a 60cm length of 32ga thermoplastic insulated hook-up wire which will interconnect to the electrode board of the recorder.

The cat is now placed in the harness assembly and the tail clamp and leg members are secured. A 30 to 60 minute period is necessary for the cat to achieve a coherent state. Determining the point when the ketamine did not affect the cat's performance was done by checking pupil dialation and observing the response of the cat when the treadmill was activated. When the cat could produce a smooth, constant gait, the recording stage of the experiment could begin. The time required from the ketamine injection to walking status averaged two hours.

Experimental Approach

Once the cat could walk, the treadmill was activated and the resulting motion of the leg along with the EMG signals were recorded by a Grass model 78 EEG/Polygraph. The six signals generated by the harness went directly in the J5 input of the Grass which produces a full scale pen deflection of 5cm for a 1 volt RMS input signal. The output of the potentiometers measuring the motion of the harness was adjusted so that the maximum travel of each potentiometer would produce a 1 volt signal. These signals produced by the harness comprise the first six channels of the Grass and represent the motion of the: (1) right ankle, (2) right knee, (3) right hip, (4) left ankle, (5) left knee, and (6) left hip.

The three EMG signals produced during each experiment were coupled to the electrode board supplied with the Grass model 78. Calibration of the three channels recording the EMG was done prior to each experiment. A representative sample of the data recorded is shown in Figure 33. The characteristic spiking of the EMG was attenuated so that the initial activity of the muscle could be distinguished more clearly. The interface with the recorder along with recording control setting is discussed in Appendix 8.

With the full harness system incorporated, the treadmill belt speed was varied to obtain data for different speeds of locomotion. Four distinct treadmill speeds were used in each experiment; 0.09 m/s, 0.19 m/s, 0.25 m/s and 0.40 m/s. In each case, the speed of the treadmill never reached the transition phase of trotting so that the cat maintained a walking gait.

To analyze the restrictive nature of the harness assembly, the above procedure was repeated for locomotion with the leg members removed and locomotion with the only support to the animal was the front paws and torso in the sling apparatus. Appendix B contains data recorded from the three variations of harness control: A - full harness, B - leg member removed but tail clamp still attached, and C - leg members and tail clamp removed.† The treadmill speed used in all variations

The recording voltage range for the EMG signals was not correlated to the physical characteristics (i.e., force, length) of the contracting muscle. All that can be determined from the EMG data is the initial activity of the muscle. However, comparative analysis can be done between the three harness configurations.

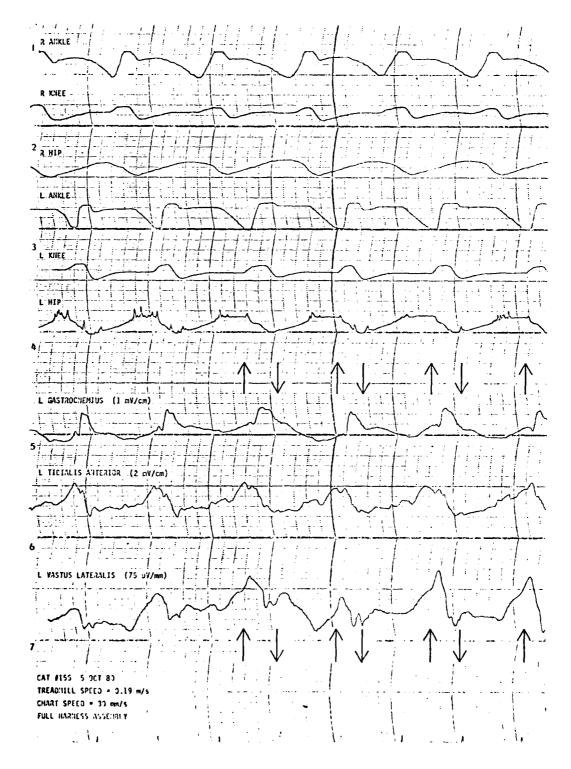


Figure 33. EMG and Position Signals

was 0.09 m/s. Because of this slow treadmill belt speed, the stance phase of the cat step cycle is about four times as long as the swing phase.

Configuration B produced a gait that was nearly identical to the gait developed in configuration A. The difference that could be seen while using configuration B was in small lateral movement of the limbs that was previously limited by the leg members in configuration A. In configuration C, the eat had to supply the posture control needed during locomotion. The cat was still in the sling assembly but the hindquarter area was not supported. The motion of the pelvis area had a small shifting (side-to-side) rhythm because of the phase difference in leg placement. However, there was no major change of the overall gait cycle when compared to A or B.

Comparing the individual EMG signals of configuration A, B and C, the basic activity of each muscle does not differ to any great extent. The peak-to-peak value for the gastrocnemius and tibialis anterior in configuration A is slightly greater than that value obtained with configurations B or C. In configuration A, the muscles of the shank must overcome the extra friction developed by the ankle pivot of the leg members which could explain the larger peak value. The distinct "spiking" of the tibialis unterior and biceps femoris in configuration C is mainly because of electrode slippage. Even with the increased activity, the basic EMG pattern of the tibialis anterior and biceps femoris developed in configuration C follows configuration A and B.

The variation of the vastus lateralis EMG between A and B is the more pronounced waveform in configuration B. Again, compensation for the harness can be seen. The spring-pully system of knee angle measurement aids in flexing the shank. The vastus lateralis must produce a slightly larger force to allow for the additional external force from the leg member system when in configuration A. Configuration C resembled that of A. The pulling force of the spring caused flexion of the shank (configuration A) and the weight of the hip area (configuration C), again causing flexion of the shank, explains the similarity of the vastus lateralis EMG of configurations A and C.

The semimembranosus activity varies little between the three configurations. The larger EMG amplitude produced in configuration C of the semimembranosus is due to the weight of the hindquarters. Since the semimembranosus is an extensor of the thigh, its rate of contraction greatly influences posture control.

EMG data recorded from the biceps femoris is extremely consistent between configurations A and B. In configuration C, the biceps femoris EMG shows bursts of activity that correspond to the peaks of the EMG developed in configurations A and B. As stated earlier, the additional noise is attributed to slippage of electrodes. The majority of the activity of the biceps femoris is during the swing phase which is very short when compared to the stance phase. To compensate for the additional weight of the pelvis area (configuration C) the biceps femoris must produce a larger force than needed when in configurations A and B.

VIII. Conclusion and Recommendations

Six muscles in the cat's rear leg that theoretically supply the contractile force needed to control basic locomotion were isolated. These muscles are: gastrocnemius and tibialis anterior (extensor and flexor of the metatarsus); vastus lateralis and biceps femoris (extensor and flexor of the shank); semimembranosus and iliopsoas (extensor and flexor of the thigh). In the full harness configuration, the three joints of the leg (i.e., hip, knee and ankle) are restricted to a single degree of freedom. That is, each joint can bend in only one plane. The individual muscles chosen provide the agonist and antagonist muscles for each joint. For the restrictive environment imposed by the harness assmebly, the six muscles will control a two-dimensional movement of the leg.

Since the data presented in this report were recorded from a healthy cat, the movement of the leg while in the harness assembly was influenced by the total array of muscles normally used during locomotion. Whether or not the six isolated muscles can produce an adequate gait cycle when the leg members are removed is an unanswered question at this time. Even with the knowledge that the six muscles chosen are either a flexor or extensor, their contractions will cause some degree of lateral and rotational movement of the leg.

When the cat is in the full harness configuration the need for posture control is eliminated. The tail clamp and sling assembly provide the support for the cat's pelvis area. This is an ideal situation

for initial attempts to induce functional motion of the leg by the computer controlled stimulators.

In each of the three harness configurations (i.e., A - full harness, B - leg members removed with tail clamp attached, C - leg members and tail clamp removed), the individual gait patterns produced by the cat during locomotion were nearly identical. However, when the tail clamp is removed, a marked difference in the EMG activity of the muscles is observed (see Appendix B). This increase in EMG amplitude and activity can be attributed to the need for active posture control during locomotion as compared to passive posture control developed during locomotion when pelvic support is provided by the tail clamp. The ability of the simplified six muscle system to provide active posture control during locomotion is dependent on the force characteristics of each muscle. Follow-on work will need to find the maximum contraction strength of each of the six muscles through tetanization. Using various modeling techniques, the forces needed for active posture control during locomotion can be determined. Comparison of the needed force to the available contractile force of the muscle under consideration will dictate whether additional muscles must be incorporated before the tail clamp can be eliminated. The force analysis work is currently being undertaken by a graduate student at the Air Force Institute of Technology (AFIT).

The eventual system that will control locomotion of a cat is shown in Figure 34. With the harness supplying the position feedback signals and the controlling muscles defined for the stimulators, the

controlling software can be developed. The computer, stimulators and assorted hardware used in this system are currently being built and integrated.

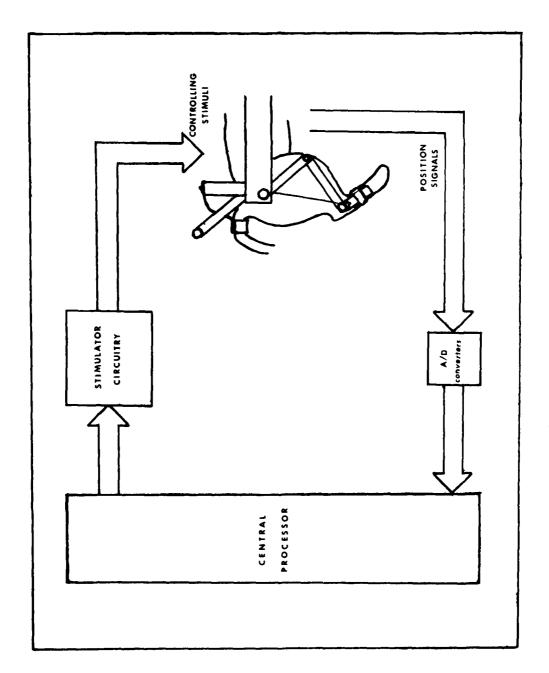


Figure 34. System Diagram

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Appendix A

The data shown in this section is used to illustrate the initial activity of the essential muscles during the gait cycle. Tables IV and V list the statistical average of the step cycle phases and initial point of muscle activity during locomotion at 0.19 m/s and 0.09 m/s respectively. Figures 35 (treadmill speed = 0.09 m/s) and 36 (treadmill speed = 0.19 m/s) illustrate the tabulated values as the leg progresses through the step cycle.

TABLE IV

Initial Activity During Step Cycle (0.19 m/s)

Muscle	\overline{X} (sec)	$\sigma(n-1)^{\dagger}$
Gastrocnemius	0.11	0.010
Tibialis Anterior	1.20	0.066
Vastus Lateralis	9.28	0.063
Semimembranosus	0.15	0.021
Biceps Femoris	1.02	0.082
Swing Phase	0.46	0.046
Stance Phase	0.97	0.069
Step Cycle	1.43	0.075

$$\dagger \sigma(n-1) = \sqrt{\frac{\Sigma(X_1 - \overline{X})^2}{n-1}}; \quad n = 15$$

TABLE V

Initial Activity During Step Cycle (0.09 m/s)

Muscle	X (sec)	o(n−1) [†]
Gastrocnemius	0.11	0.015
Tibialis Anterior	1.88	0.121
Vastus Lateralis	0.27	0.025
Semimembranosus	0.14	0.039
Biceps Femoris	1.48	().191
Swing Phase	0.54	0.042
Stance Phase	1.43	0.096
Step Cycle	1.97	0.091

$$f_{\sigma(n-1)} = \sqrt{\frac{\sum (X_4 - \bar{X})^2}{n-1}}; n = 10$$

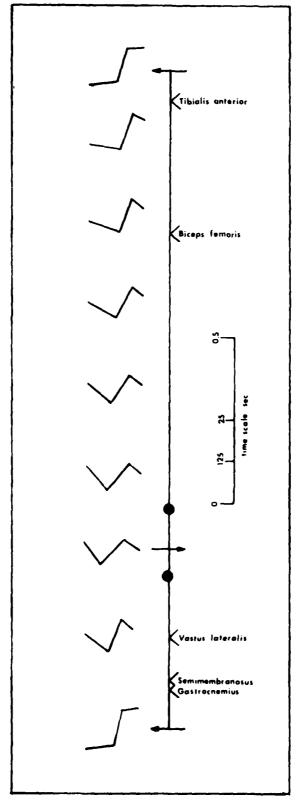


Figure 35. E.G vs. Step Cycle (0.09 m/s)

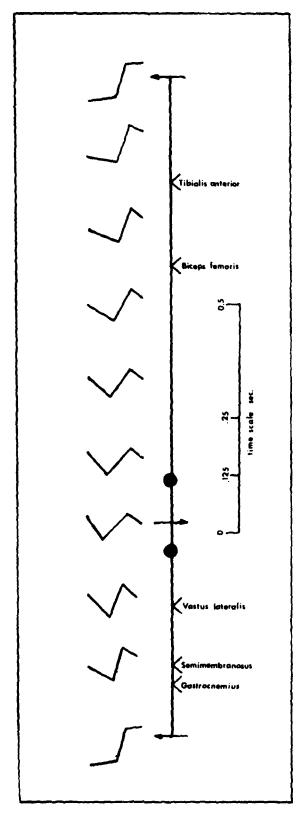


Figure 36. EMG vs. Step Cycle (0.19 m/s)

Appendix B

This section contains additional experimental data. With the cat in the full harness configuration (A), EMG data from the essential muscles is shown for the four different treadmill belt speeds (i.e., 0.09 m/s, 0.19 m/s, 0.25 m/s and 0.40 m/s). EMG data developed in the two other harness configurations (i.e., leg members removed but tail clamp attached (B), and both leg members and tail clamp removed (C)) is shown for the treadmill belt speed of 0.09 m/s.

The EMG signal from each muscle went through a filter exhibiting the characteristics shown in Figure 37. The maximum frequency of the recording pens, set at 30 Hz, produced a smooth, distinct waveform. This uncluttered waveform showed initial low frequency activity of the muscle. High frequency EMG signals produced during strong muscular contraction are attenuated by the low pass filter (LPF). This can be seen in the attenuated EMG waveform of the gastrochemius during the stance phase of the step cycle when the majority of contractile force is produced.

The integrated appearance of the EMG waveforms is attributed to the LPF characteristics. With a fall time constant of 250 ms, the LPF behaves as a crude integrator. The integration performed by the LPF explains the absence of characteristic "spiking" of EMG signals.

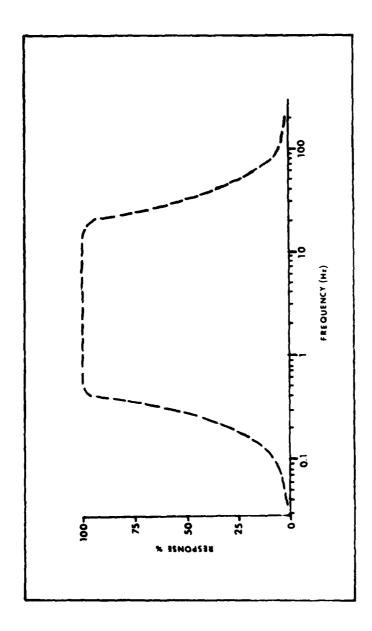


Figure 37. Frequency Band Fass of EG Recorder

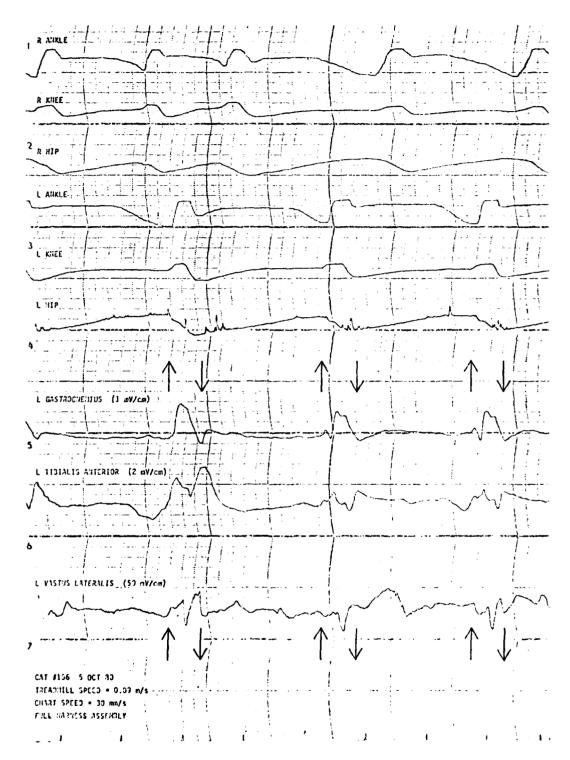


Figure 38. Experimental Data: Configuration A (0.09m/s)

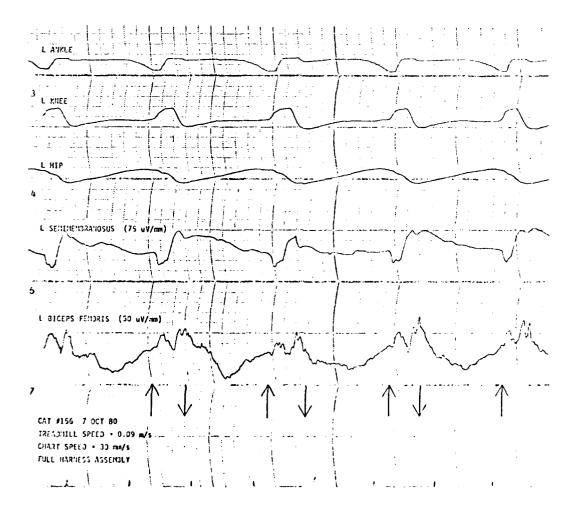


Figure 38b

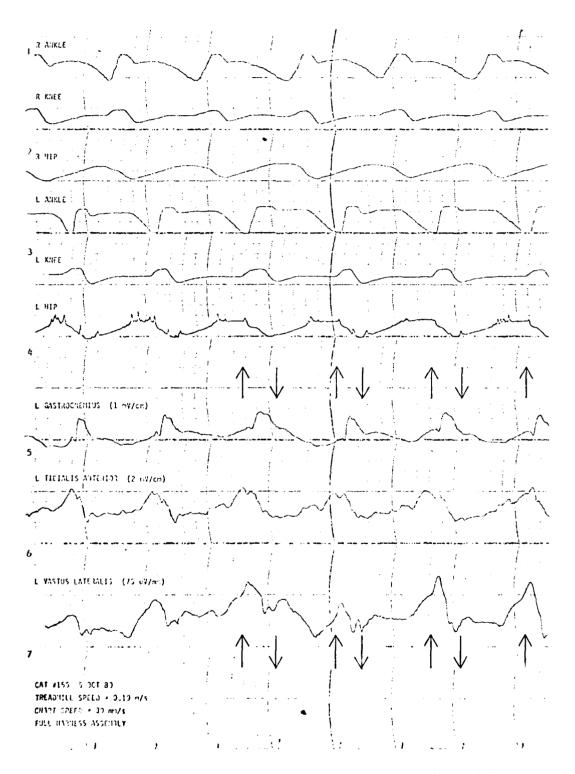


Figure 39. Experimental Data : Configuration A (0.19m/s)

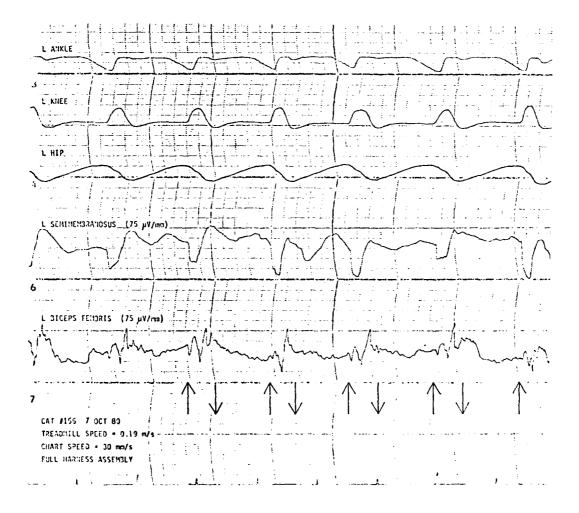


Figure 395

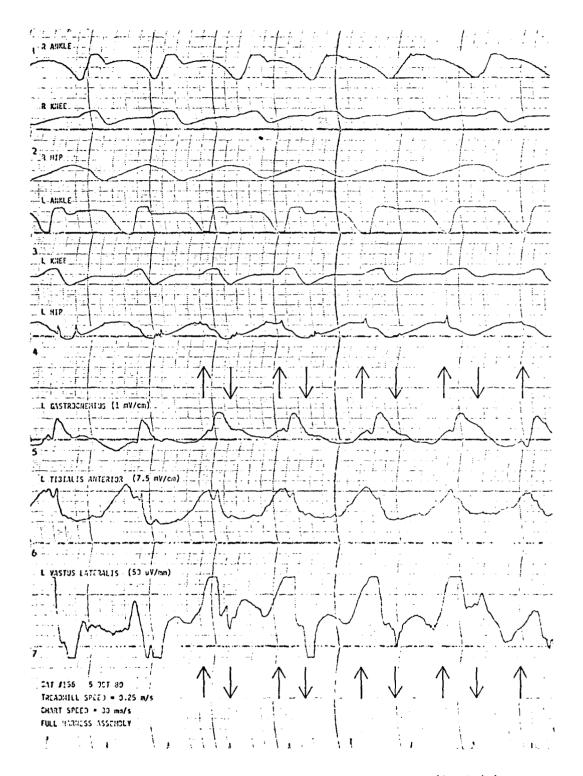


Figure 40. Experimental Data: Configuration A (0.25m/s)

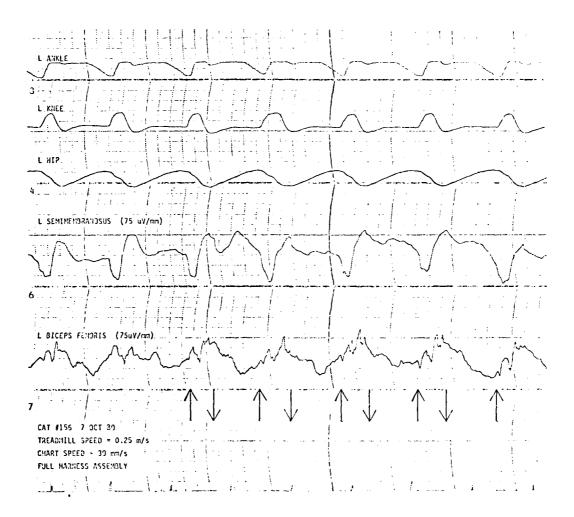


Figure 40b

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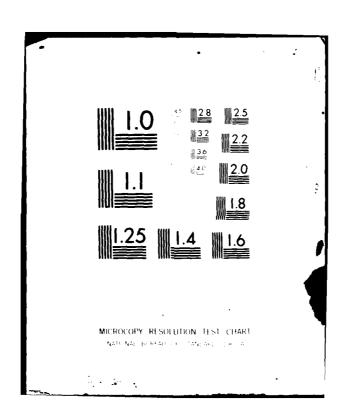
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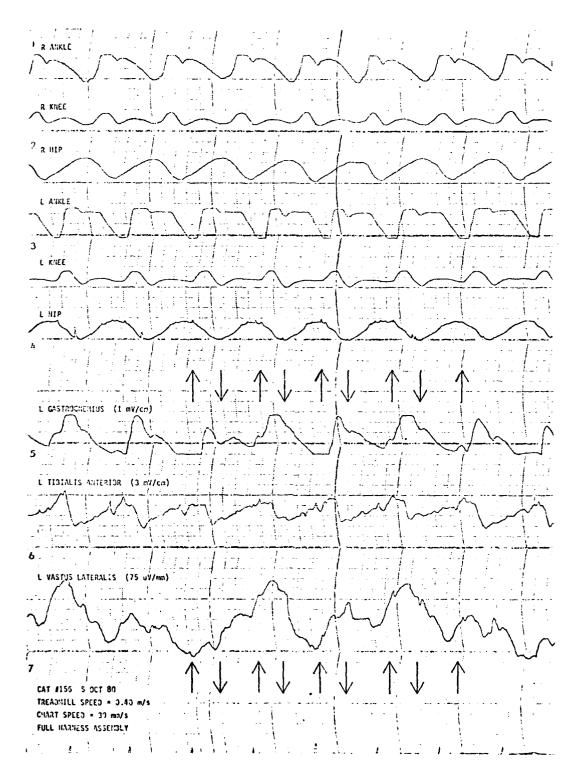


Figure 41. Experimental Data: Configuration A (0.40m/s)

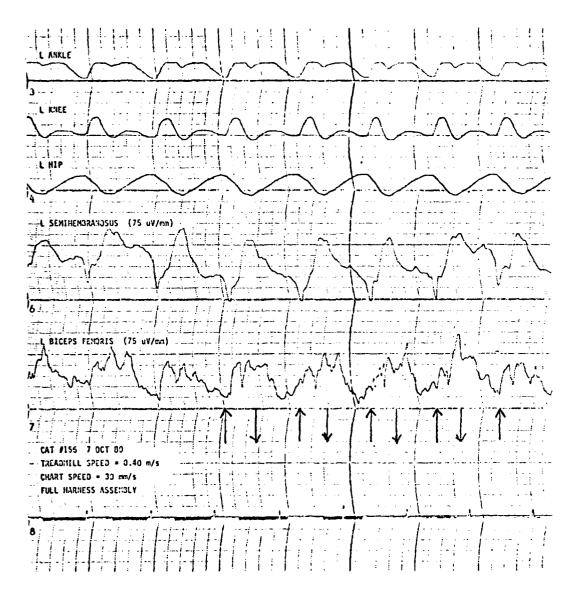


Figure 41b

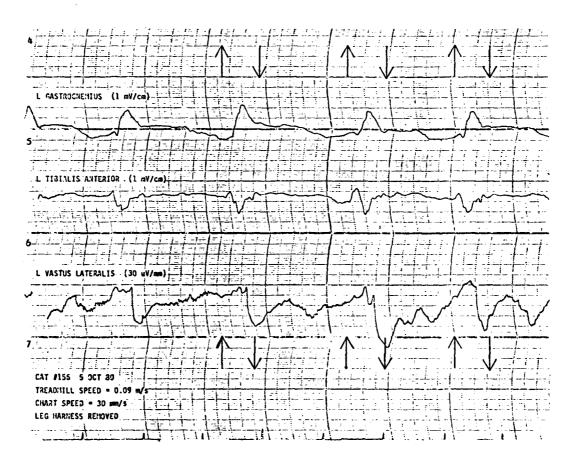


Figure 42. Experimental Data: Configuration B (0.09m/s)

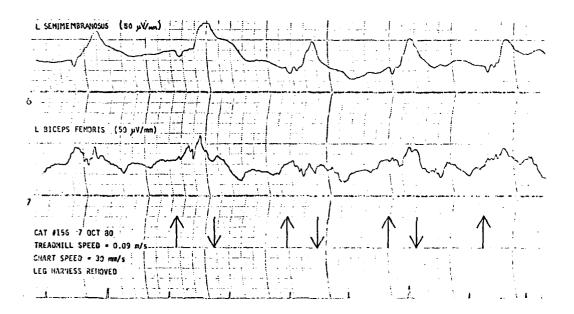


Figure 42b

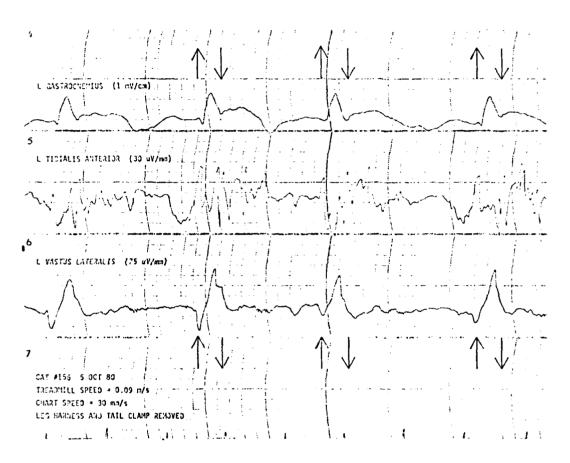


Figure 43. Experimental Data: Configuration C (0.09m/s)

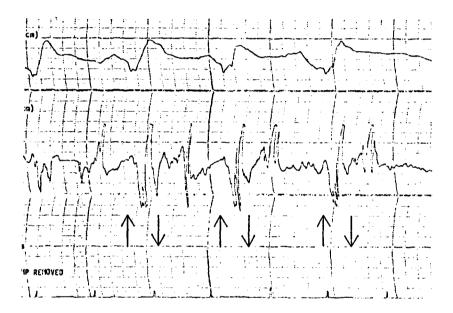


Figure 43b

